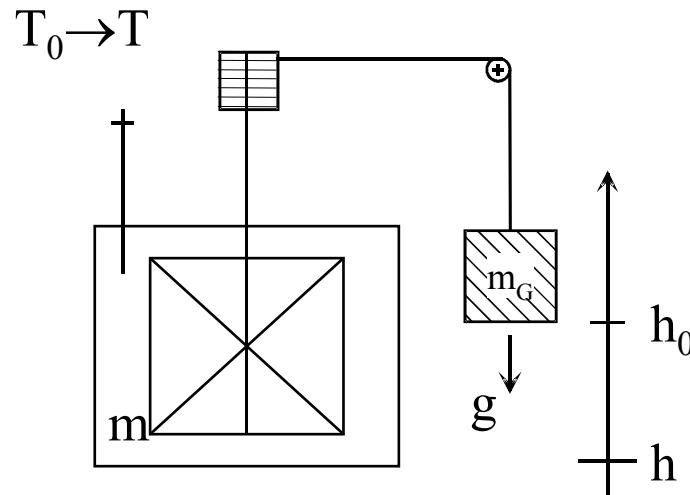
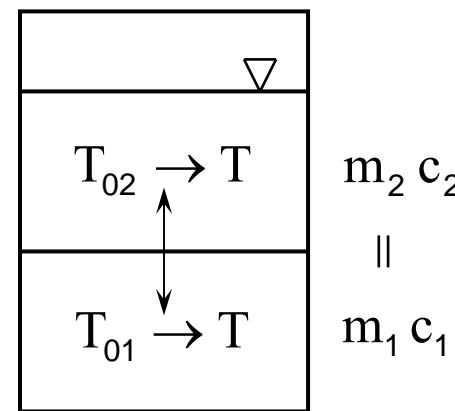


## Irreversibility of Processes in Closed System

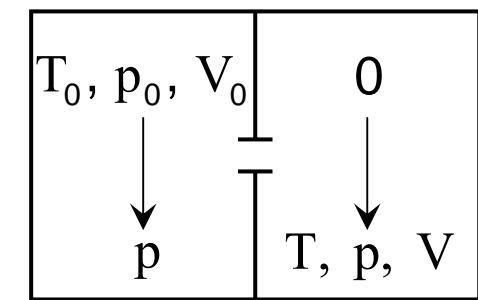


J.P. Joule  
Stirring experiment

$$m_G g (h_0 - h) = m c_v (T - T_0) \geq 0 \quad T_{01} - T = T - T_{02} \geq 0 \quad U(T_0, V_0, m) = U(T, V_0 + V, m)$$



J.B. Fourier  
Heat transfer



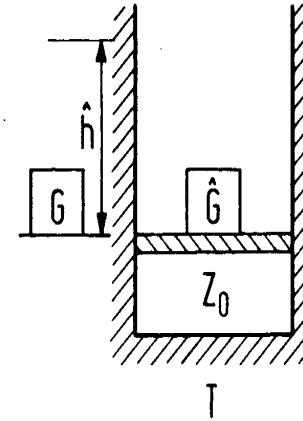
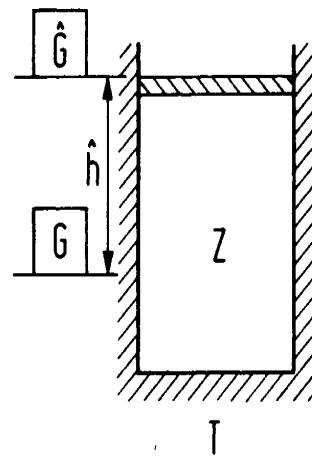
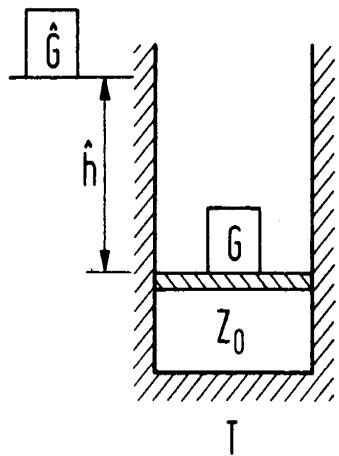
Gay-Lussac  
Gas expansion

$$V \geq 0$$

$$\text{I.G.: } T_0 = T$$

## Gas Expansion Process

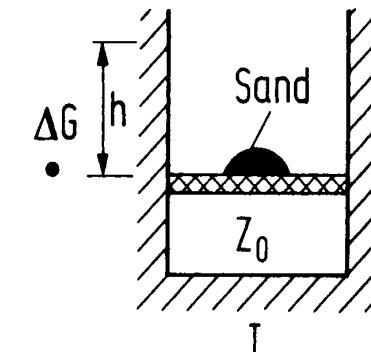
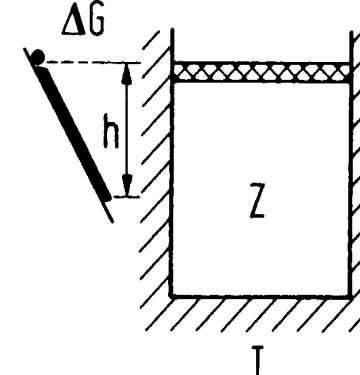
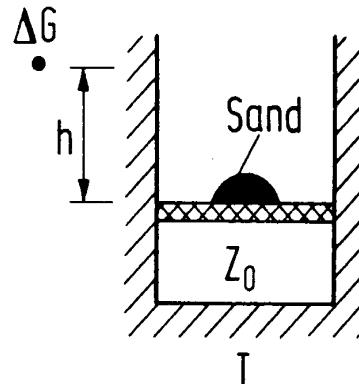
### Irreversibility



VELO	$> 0$
Z	NEQ
$\Sigma^*$	$\neq \Sigma^*$
REV	$F > 0$

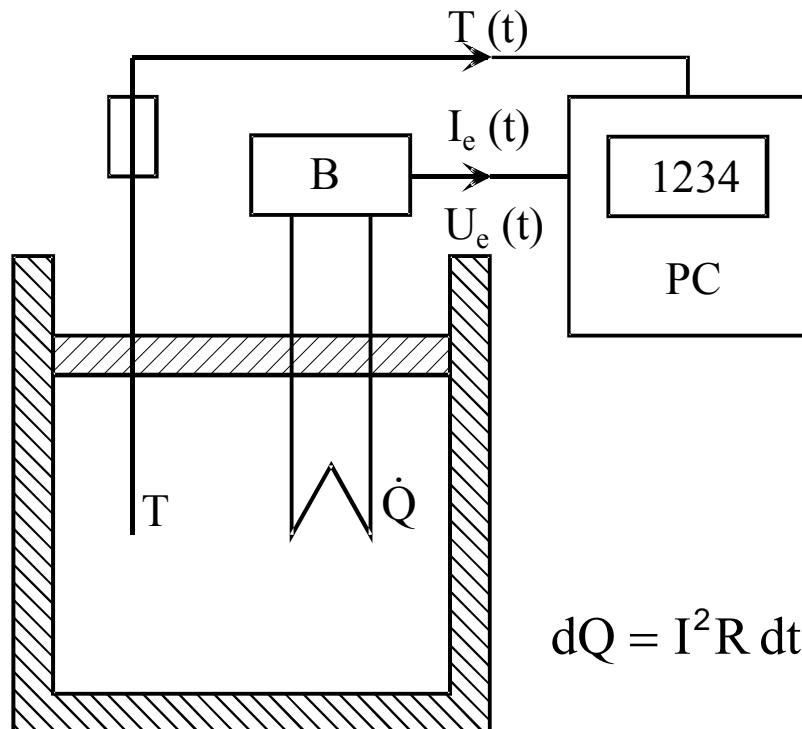
### Reversibility

VELO	$\theta$
Z	EQ
$\Sigma^*$	$= \Sigma^*$
REV	$F = 0$



## 2<sup>nd</sup> Law (1): Clausius Entropy

$$S(Z) = S(Z_0) + \oint_{Z_0} \frac{dQ_{\text{rev}}}{T} \dots dT \rightarrow 0$$



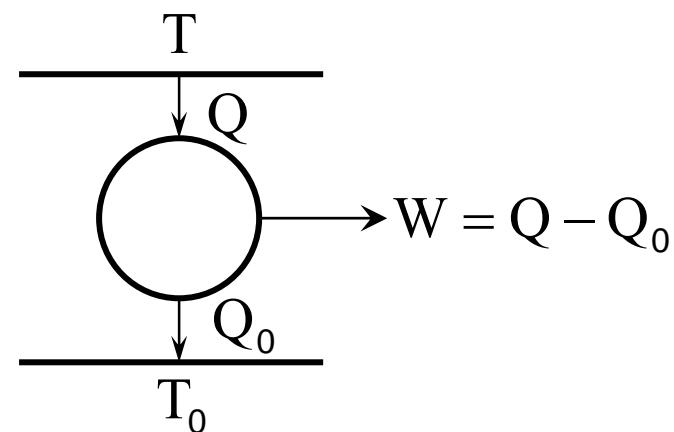
Entropymeter

Clausius Equality ( $Z = Z_0$ )

$$0 = \oint \frac{dQ_{\text{rev}}}{T}$$

Carnot-Relation

$$\frac{Q}{T} = \frac{Q_0}{T_0} , \quad \eta_c = \frac{W}{Q} = 1 - \frac{T_0}{T}$$



## Gibbs Equation (Simple System)

1<sup>st</sup> Law :

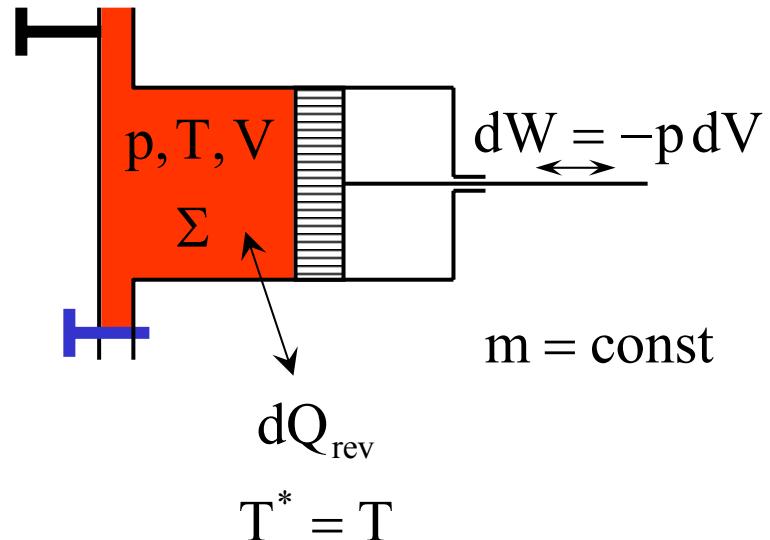
$$dU = dQ_{rev} - p dV$$

2<sup>nd</sup> Law:

$$dS = dQ_{rev} / T$$

Gibbs:

$$dS = \frac{1}{T} dU + \frac{p}{T} dV$$



$$T^* = T$$

$$\left( \frac{\partial^2 S}{\partial T \partial V} \right) = \left( \frac{\partial^2 S}{\partial V \partial T} \right) \rightarrow S = S_0 + \int_{T_0(V_0)}^T \frac{C_{V_0}}{T'} dT' + \int_{V_0(T)}^V \left[ \frac{\partial p(T, V')}{\partial T} \right]_T dV'$$

Caloric EOS   Thermal EOS

## Entropy of Ideal Substances

Ideal Gas

$$\text{TEOS: } pV = \left(\frac{m}{M}\right)RT$$

$$\text{CEOS: } H = H_0 + mc_p(T - T_0)$$

$$\rightarrow S = S_0 + m \left[ c_p \ln\left(\frac{T}{T_0}\right) - \frac{R}{M} \ln\left(\frac{p}{p_0}\right) \right]$$

$$\rightarrow S = S_0 + m \left[ c_v \ln\left(\frac{T}{T_0}\right) + \frac{R}{M} \ln\left(\frac{V}{V_0}\right) \right]$$

Ideal Liquid

$$\text{TEOS: } \rho = \text{const} = 1/v$$

$$\text{CEOS: } c = \text{const}$$

$$H = H_0 + mc(T - T_0) + mv(p - p_0)$$

$$S = S_0 + mc \ln\left(\frac{T}{T_0}\right)$$

$$S(U, n_1 \dots n_N) = S^* + \sum_{i=1}^N c_{i0} \ln \left( 1 + \frac{U - U^*}{c n T^*} \right) n_i$$

$$S(U^*, n_1 \dots n_N) \equiv S^* = \sum_{i=1}^N (s_{i0}^* - R \ln x_i) n_i$$

$$G(T, n_1 \dots n_N) = G^* + \sum_{i=1}^N \left[ (c_{i0} - s_{i0}^* + R \ln x_i)(T - T^*) - c_{i0} T \ln \left( \frac{T}{T^*} \right) \right] n_i$$

$$G(T^*, n_1 \dots n_N) \equiv G^* = \sum_{i=1}^N (-s_{i0}^* + R \ln x_i) T^* n_i + U^* + pV$$

$$U = \sum_i U_{i0} = U^* + \sum_{i=1}^N c_{i0} (T - T^*) n_i, V = \sum_{i=1}^N v_{i0} n_i$$

$$H = \sum_i H_{i0} = H^* + \sum_{i=1}^N [c_{i0} (T - T^*) + p v_{i0}] n_i$$

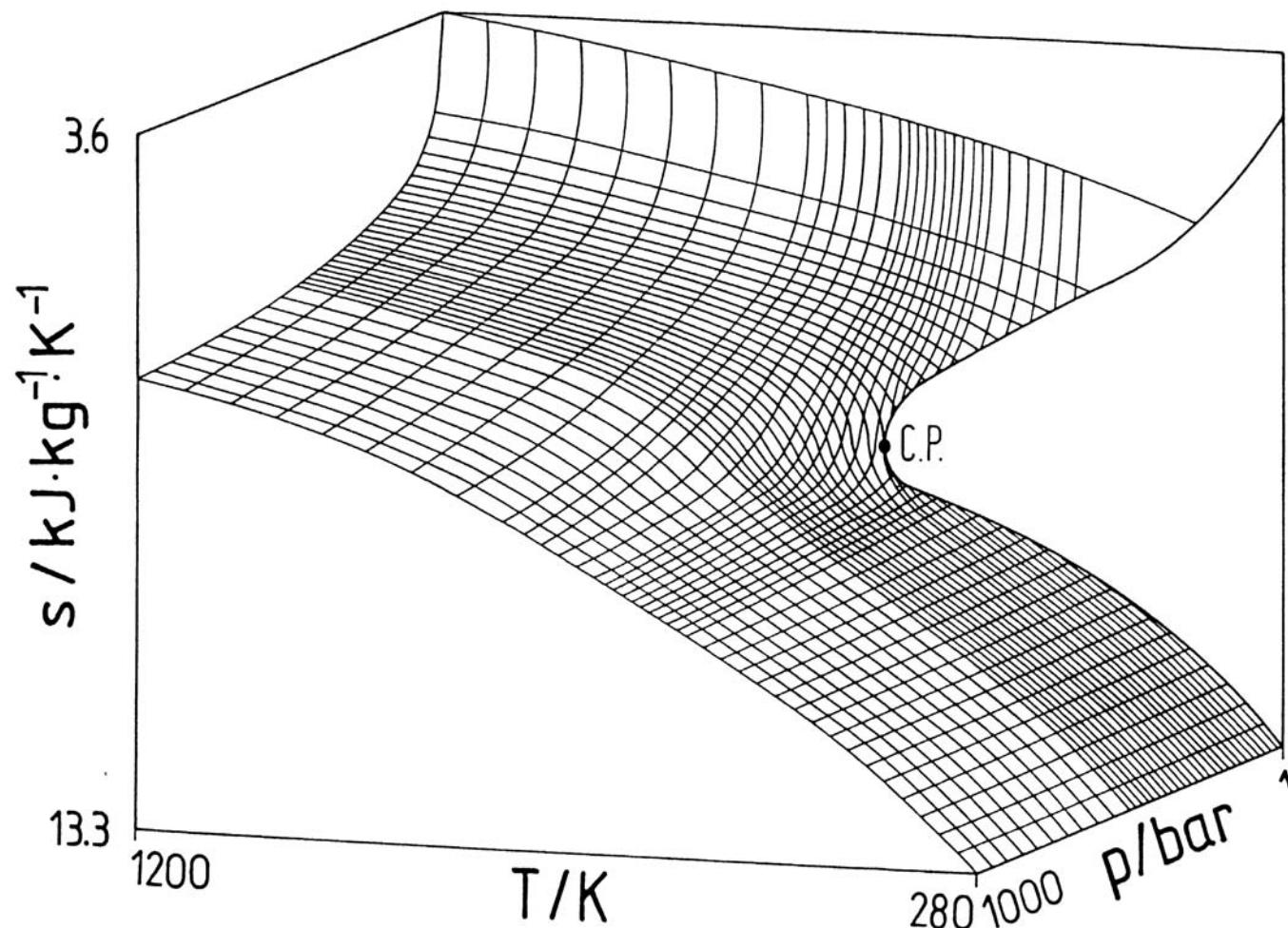
$$\mu_i(T, n_1 \dots n_N) = \mu_i^* + (T - T^*) s_{i0}^* + c_{i0} T \ln \left( \frac{T}{T^*} \right) - R(T - T^*) \ln x_i$$

$$\mu_i(T^*, n_1 \dots n_N) \equiv \mu_i^* = T^* s_{i0}^* - R T^* \ln x_i$$

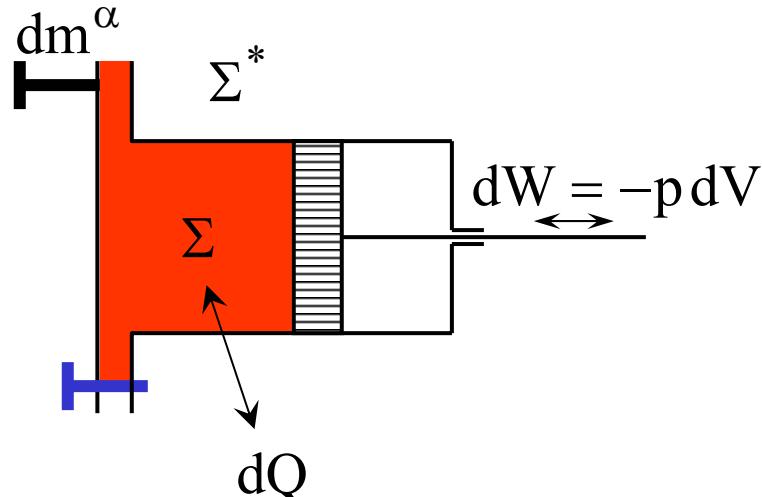
**Incompressible, ideal fluid mixture ( $c_{i0} = \text{const}, v_{i0} = \text{const}, i = 1 \dots N$ )**

## Entropy of Water ( $\text{H}_2\text{O}$ )

K. Stephan, W. Wagner  
IAPS (1985)



## 2<sup>nd</sup> Law (2): Clausius Inequality



Exchange of  
mass      heat      work

$$\Sigma : Z_0 \rightarrow Z$$

$$\begin{aligned} \text{IRR} : S - S_0 &\geq \oint_{Z_0}^Z \left( \frac{dQ}{T^*} + \sum_{\alpha} s^{(\alpha)} dm^{(\alpha)} \right) \\ \text{REV} : \end{aligned}$$

Quasistatic changes of state ( $Z \rightarrow Z + dZ$ )

$$dS \geq \frac{dQ}{T^*} + \sum_{\alpha=1}^A s^{(\alpha)} dn^{(\alpha)}$$

Closed Systems:  $dQ = 0$ ,  $dm^{(\alpha)} = 0$

$\text{IRR} : S \geq S_0 \dots$  World Statement?  
 $\text{REV} :$

## Interpretations of the Clausius Entropy ( $S(Z)$ )

### 1. M. Planck (1885)

Measure for “probability”, tendency, preference of a system to actually realize a certain equilibrium state ( $Z$ ).  
( $N_2$ -gas in steel bottle)

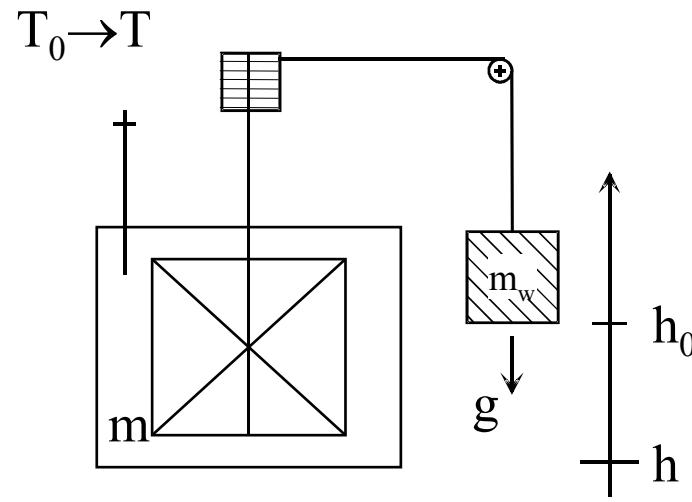
### 2. L. Boltzmann (1890)

Measure for molecular “disorder” in a system in state ( $Z$ ).  
(Crystal, liquid, gas, plasma ...)

### 3. C. Shannon (1948)

Measure for “lack of knowledge” of the micro- i.e. molecular state of a system ( $\Sigma$ ) in a given macroscopic state ( $Z$ )

## Stirring Experiment of J.P Joule



$$1^{\text{st}} \text{ Law: } U_0 + m_w g h_0 = U + m_w g h$$

$$\text{CEOS: } U = U_0 + m c_v (T - T_0)$$

$$2^{\text{nd}} \text{ Law (1), I.G.:}$$

$$S = S_0 + m c_v \ln\left(\frac{T}{T_0}\right)$$

$$Z_0 : T_0, h_0$$

$$2^{\text{nd}} \text{ Law (2):}$$

$$\underline{S > S_0}$$

$$\frac{Z : T, h}{Z_0 \rightarrow Z}$$

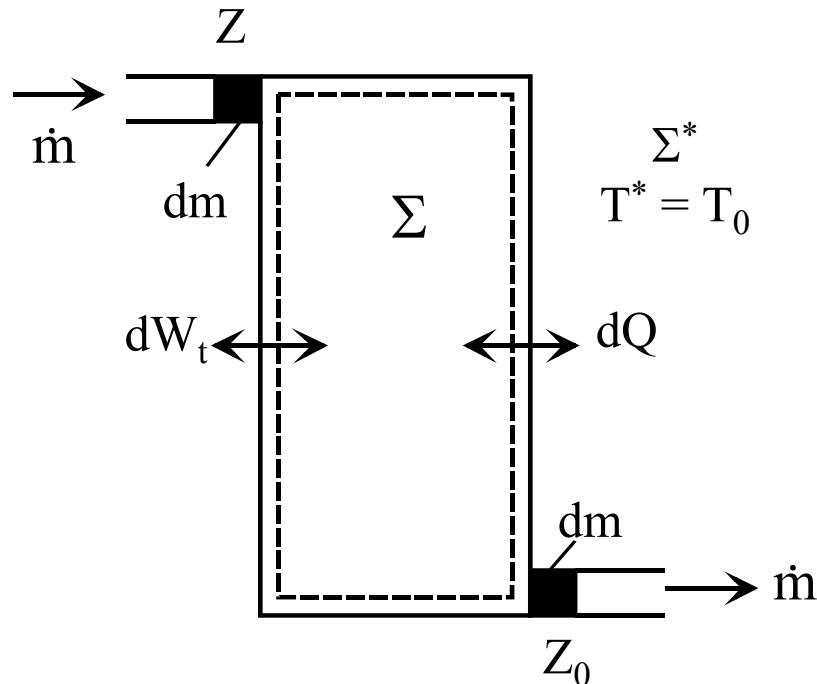
$$\rightarrow T > T_0$$

$$\underline{\rightarrow h < h_0}$$

Reversed process  $(T < T_0, h > h_0)$  not possible!

## Maximum Work of a Mass Flow (H. von Helmholtz (1890))

Simple open system ( $Z \rightarrow Z_0$ )



$Z$ :  $h, s, T, p, \rho$

$Z_0$ :  $h_0, s_0, T_0 = T^*, p_0, \rho_0$

Stationary State ( $\dot{Z} = 0$ )

$$1^{\text{st}} \text{ Law : } \dot{U} = \dot{Q} + \dot{W}_t + (h - h_0) \dot{m} = 0$$

$$2^{\text{nd}} \text{ Law: } \dot{S} = \frac{\dot{Q}}{T^*} + (s - s_0) \dot{m} + P_s = 0$$


---

$$P_s \geq 0$$

$$-\dot{W}_t = [h - h_0 - T^*(s - s_0)] \dot{m} - T^* P_s$$

$$-\dot{W}_t = e_x(Z, Z_0) \dot{m} + P_{\text{ex}}$$


---

$$P_{\text{ex}} = -T^* P_s \leq 0$$

## Thermodynamics of Processes (1)

Discrete System, Exchange of Heat, Work, Mass

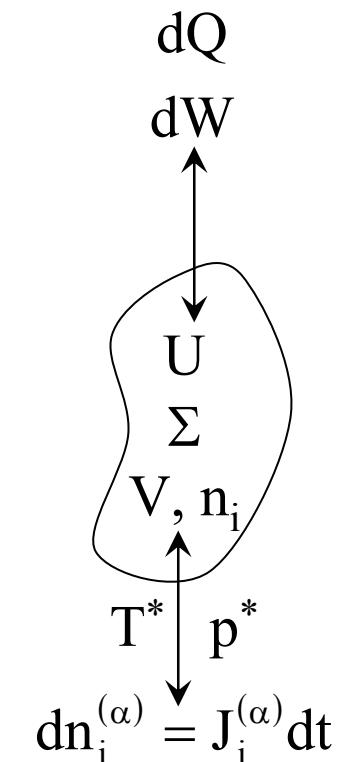
Balance Equations :  $\dot{n}_i = \sum_{\alpha} \dot{n}_i^{(\alpha)}$

$$\dot{U} = \dot{Q} - p^* \dot{V} + \sum_{\alpha} h^{(\alpha)} \dot{n}^{(\alpha)}$$

Gibbs Equation :  $dS = \frac{1}{T} dU + \frac{p}{T} dV - \sum_i \mu_i dn_i$

Clausius Inequality :  $S - S_0 = \int_{Z_0}^Z \left( \frac{dQ}{T^*} + \sum_{\alpha} s^{(\alpha)} dn^{(\alpha)} \right)$

Fundamental Inequality:



(\*)  $\int_0^t \left[ \left( \frac{1}{T} - \frac{1}{T_*} \right) \dot{U} + \left( \frac{p}{T} - \frac{p^*}{T^*} \right) \dot{V} + \sum_{i,\alpha} \left( \frac{\mu_i^{(\alpha)}}{T^{(\alpha)}} - \frac{\mu_i}{T} \right) \dot{n}_i^{(\alpha)} \right] dt \geq 0 \dots \text{all } (t)$

Thermal energy

work

mass exchange

## Process Equations (Flux-Force-Relations)

(Eckart – Onsager – Meixner – Prigogine)

Thermal energy  $\dot{U}(t) = F_u(\%)$

Heat transfer

Mechanical work  $\dot{V}(t) = F_v(\%)$

Mass transfer  $\dot{n}_i^{(\alpha)}(t) = F_i^{(\alpha)}(\%) \quad i = 1 \dots N, \alpha = 1 \dots A$

$$(\%) = \left( \frac{1}{T} - \frac{1}{T^*}, \frac{p}{T} - \frac{p^*}{T^*}, \frac{\mu_k^{(\alpha)}}{T^{(\alpha)}} - \frac{\mu_k}{T}, k = 1 \dots N, \alpha = 1 \dots A \right)$$

F ... Functions or Functionals ( $-\infty \leq s \leq t$ ) of  
their arguments

## Classification of Process Equations

	Linearity	Non-Linearity
Function (t)	TIP	NTIP
F(%)	LPS	NPS (?)

Fundamental Inequality (2<sup>nd</sup> Law, (\*))  
Theorem (JUK, 1968)

$$\int_0^t \sum_i \dot{x}_i F_i(\underline{x}, \dot{\underline{x}}) dt \geq 0 \dots \text{all } t \geq 0$$

$$F_i(\underline{x}, \dot{\underline{x}} = 0) = 0 , i = 1 \dots N$$

$$\rightarrow P_s = \sum_i \dot{x}_i F_i(\underline{x}, \dot{\underline{x}}) \geq 0$$

### TIP

$$F_i(\underline{x}, \dot{\underline{x}}) = \sum_k^N L_{ik}(\underline{x}) \dot{x}_k$$

Onsager-Casimir-Relations

$$L_{ik} = \varepsilon_i \varepsilon_k L_{ki} , \varepsilon_i, \varepsilon_k = \pm 1$$

### NTIP

$$F_i(\underline{x}, \dot{\underline{x}}) = \sum_k^N L_{ik}(\underline{x}) \dot{x}_k + \\ + \sum_{klm} M_{iklm}(\underline{x}) \dot{x}_k \dot{x}_l \dot{x}_m + 0 \quad (5)$$

### LPS

$F_i(\underline{x}, \dot{\underline{x}})$  ... Linear Passive Functional  
(J. Meixner, H. König, 1964)

# **Dimensional Analysis**

## **Phenomenological Coefficients and Functions:**

## Buckingham's Theorem ( $\pi$ – Theorem):

$$Y = Y(Z_1 \dots Z_M)$$

## Basic Units System (SI-System)

$$G_1, G_2, \dots G_g$$

$$\rightarrow Y = \prod_{i=1}^M Z_i^{\alpha_i} \phi(\pi_1 \dots \pi_{M-r})$$

$$[Y] = \left[ \begin{array}{c} M \\ \prod_{i=1}^M Z_i^{\alpha_i} \end{array} \right]$$

$$\pi_k = \prod_{j=1}^M Z_j^{\beta_{jk}} , \quad [\pi_k] = 1$$

$$\ln \phi = \phi_0 + \sum_{j=1}^{\mu-r} \phi_{1i} \ln \pi_i + \dots$$

## Dimensional Matrix

	Z <sub>1</sub>	.....	Z <sub>M</sub>
G <sub>1</sub>	ζ <sub>11</sub>	.....	ζ <sub>1M</sub>
·	·		
·	·		Rank:
·	·	r	
·	·		
·	·		
·	·		
G <sub>g</sub>	ζ <sub>g1</sub>	.....	ζ <sub>gM</sub>

## Dimensional Analysis

Taylor series expansion of the reduced function  $\phi(\pi_1 \dots \pi_{M-r})$ :

$$\ln \phi(\pi_1 \dots \pi_{M-r}) = \psi(\ln \pi_1 \dots \ln \pi_{M-r}) \quad \dots \pi_i \geq 0$$

$$= \psi_0 + \sum_i^{M-r} \beta_i \ln \pi_i + \sum_{i,k}^{M-r} \gamma_{ik} \ln \pi_i \cdot \ln \pi_k + O(3)$$

$$\phi(\pi_1 \dots \pi_{M-r}) = C \prod_i^{M-r} \pi_i ** \left( \beta_i + \sum_k \gamma_{ik} \ln \pi_k + \sum_{k,l} \delta_{ikl} \ln \pi_k \cdot \ln \pi_l + \dots \right)$$

$$\cong C \prod_i^{M-r} \pi_i^{\beta_i} \prod_i^{M-r} \pi_i^{\sum_k \gamma_{ik} \ln \pi_k} \dots , \quad C \doteq e^{\psi_0}$$

Energy: Scale shift invariance!

## Example 1: Velocity of Molecules in an Ideal Gas

List of “relevant” variables, parameters, constants:

$$w = w(T, p, V_m, M, R)$$

	T	p	$V_m = V/N$	M	R	
m		-1	3		2	$M = 5$
s		-2			-2	$G = 5$
kg		1		1	1	$r = 5$
K	1				-1	$\overline{M - r = 0}$
kmol			-1	-1	-1	

$$w = \sqrt{\frac{RT}{M}} \cdot \text{Const} \quad , \quad \text{Calibration Experiment: Const} = \sqrt{3} \quad , \quad w = \sqrt{\frac{3RT}{M}}$$

## Process Calculation (Initial value problem, ODE)

$$\rightarrow \Sigma : Z(t) = \left( U(t), V(t), n_i(t) = \sum_{\alpha}^A n_i^{(\alpha)} \right)$$

Accompanying equilibrium intensive parameters at time (t):

$$S = S(U, v, n_1, \dots, n_N)$$

$$dS = \frac{1}{T} dU + \frac{p}{T} dV - \sum_i^N \frac{\mu_i}{T} dn_i$$

$$\rightarrow T(t), p(t), \mu_i(t)$$

Process equations for  $\dot{U}, \dot{V}, \dot{n}_i$ , Taylor-series expansion:

$$\Sigma : Z(t + \Delta t) = \left( U(t + \Delta t) = U(t) + F_u(t)\Delta t + \frac{1}{2}\dot{F}_u(\Delta t)^2 + \dots \right)$$

...

$$\dot{n}_i^{(\alpha)}(t + \Delta t) = \dot{n}_i^{(\alpha)}(t) + F_i^{(\alpha)}(t)\Delta t + \frac{1}{2}\dot{F}_i^{(\alpha)}(t)(\Delta t)^2 + \dots \right)$$

Iteration procedure

## Stationary Processes and States

$$\dot{U} = 0, \dot{V} = 0$$

$$\dot{n}_i = \sum_{\alpha=1}^A \dot{n}_i^{(\alpha)}, \quad i = 1 \dots N$$

Fundamental Inequality (\*)

$$P_s = \sum_{i,\alpha}^{N,A} \left( \frac{\mu_i^{(\alpha)}}{T^*} - \frac{\mu_i}{T} \right) \dot{n}_i^{(\alpha)} \geq 0$$

Process Equations (Flux – Force – Relations)

Mass transfer:  $\dot{n}_i^{(\alpha)} = F_i^{(\alpha)}(./.), \quad i = 1 \dots N, \alpha = 1 \dots A$

---

$$(./.) = \left( \frac{\mu_i^{(\alpha)}}{T^*} - \frac{\mu_i}{T}, \quad i = 1 \dots N, \alpha = 1 \dots A \right)$$