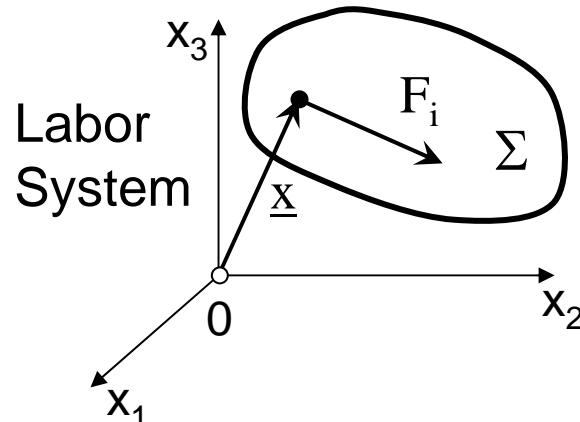


## Classical Theory (3): Thermostatics of Continuous Systems with External Forces



$\Sigma$ : Equilibrium State?

Isolation, Inhomogeneity

External Forces  $F_{i\alpha} = -\partial_\alpha \varphi_i(\underline{x})$

Components:  $i = 1 \dots N$

$$S = \int_v S_v(\underline{x}) dV \rightarrow \text{Max.}$$

$$U + W_p = \int_v \left[ U_v(\underline{x}) + \sum_{i=1}^N \rho_i(\underline{x}) \varphi_i(\underline{x}) \right] dV = \text{const}$$

$$m_i = \int_v \rho_i(\underline{x}) dV = \text{const}_i, i = 1 \dots N$$

Equilibrium Conditions:

$$T(\underline{x}) = \text{const}$$

$$\partial_\alpha p(\underline{x}) = \sum_i^N \rho_i(\underline{x}) F_{i\alpha}$$

$$\mu_i(\underline{x}) + \varphi_i(\underline{x}) = \text{const}_i, i = 1 \dots N$$

Boundary Conditions

Generalizations: E-M-Fields

Chem. Reactions

Ref.: J.U. Keller, TIP, Part 1

Thermostatics, W. de Gruyter,  
Berlin - New York, 1977.

## Thermodynamics of Processes (2)

Continuous System

Fluid,  $N \geq 1$  Components

External Forces

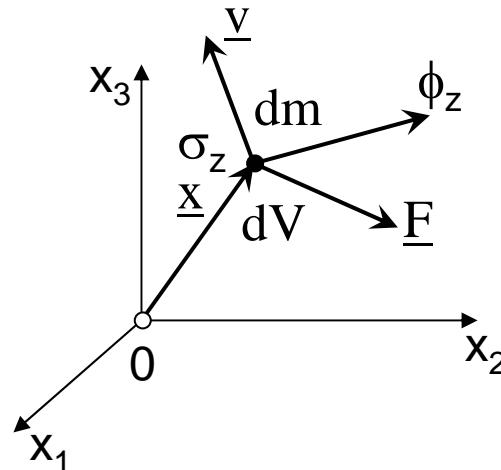
Extensive Quantity (Z)

$$\begin{aligned} Z(t) &= \int_V z_V(\underline{x}, t) dV(\underline{x}) \\ &= \int_m z_m(\underline{x}, t) dm(\underline{x}) \end{aligned}$$

$$z_m(\underline{x}, t) = \rho(\underline{x}, t) z_V(\underline{x}, t)$$

Balance Equation

$$\dot{Z} = \Phi + P$$



Local Formulation (Lab)

$$\partial_t z_V + \partial_\alpha \phi_{z\alpha} = \sigma_z$$

Material Formulation

$$\rho d_t z_m + \partial_\alpha (\phi_{z\alpha} - \rho v_\alpha z_m) = \sigma_z$$

$$d_t \equiv \frac{d}{dt} = \partial_t + v_\alpha \partial_\alpha, \quad \partial_t = \frac{\partial}{\partial t}, \quad \partial_\alpha = \frac{\partial}{\partial x_\alpha}$$

## Balance Equations of Mass Densities

$$\rho_i(\underline{x}, t), i = 1 \dots N$$

Partial density of component (i)

$$Z: z_v = \rho_i, z_m = w_i$$

$$\phi_z = \rho_i v_i, \sigma_z = \Gamma_i$$

$$\rho(\underline{x}, t) = \sum_i^N \rho_i(\underline{x}, t)$$

Total mass density

$$w_i = \rho_i / \rho$$

Mass concentration (i)

Local balance

$$v_i(\underline{x}, t)$$

Partial velocity

$$\frac{\partial_t \rho_i + \partial_\alpha (\rho_i v_{i\alpha})}{\partial_t \rho_i + \partial_\alpha (\rho_i v_{i\alpha})} = \Gamma_i$$

$$v = \sum_i w_i v_i$$

Velocity of mass element  $\Delta m(\underline{x}, t)$

Material balance

$$\Gamma_i, i = 1 \dots N$$

Chemical production rate (i)

$$\rho \frac{d}{dt} w_i + \partial_\alpha J_{i\alpha} = \Gamma_i$$

$$\sum_i \Gamma_i = 0$$

Mass conservation

$$J_{i\alpha} = \rho_i (v_{i\alpha} - v_\alpha)$$

Diffusion flow (i)

## Balance Equation of Linear Momentum

$P_{\alpha\beta}(\underline{x}, t)$  Stress Tensor

$\beta$ -component of stress  
at  $\alpha$ -surface element

$F_i(\underline{x}, t)$  External force acting on  
component (i)

Z:  $z_v = \rho v_\alpha, z_m = v_\alpha$

Newton's equation of motion of mass (m)

$$\frac{d}{dt} \int_{V(t)} \rho v_\alpha dV = - \oint_{O(t)} P_{\alpha\beta} dO_\beta + \int_{V(t)} \sum_i^N \rho_i F_{i\alpha} dV$$

Material balance

$$\rho \frac{d}{dt} v_\alpha + \partial_\beta P_{\alpha\beta} = \sum_i^N \rho_i F_{i\alpha}$$

$\alpha = 1, 2, 3$

Local balance

$$\partial_t (\rho v_\alpha) + \partial_\beta (P_{\alpha\beta} + \rho v_\alpha v_\beta) = \sum_i^N \rho_i F_{i\alpha}$$

$\alpha = 1, 2, 3$

Internal stress

Convective flow  
of momentum

## Balance Equation of Angular Momentum (AM)

$z_m = \varepsilon_{\alpha\beta\gamma} x_\beta v_\gamma + \sigma_\alpha$  Specific angular momentum ( $\alpha$ ) at  $(\underline{x}, t)$   
 $\alpha = 1, 2, 3$

$\varepsilon_{\alpha\beta\gamma} = (1, -1, 0)$  Antisymmetric unit-tensor

$\sigma_\alpha$  Internal angular momentum (IAM)  
(Spin of atoms, molecules etc.)

$\sum_{\alpha\beta}$  Tensor of IAM-flux

$\Gamma_\alpha$  Production density of IAM due to external forces

Momentum balance  $(\alpha \rightarrow \gamma) / \varepsilon_{\alpha\beta\gamma} x_\beta$ , IAM

$$\rho \frac{d}{dt} (\varepsilon_{\alpha\beta\gamma} x_\beta v_\gamma + \sigma_\alpha) + \partial_\delta (\varepsilon_{\alpha\beta\gamma} x_\beta P_{\gamma\delta} + \sum_{\alpha\delta}) =$$

$$= \varepsilon_{\alpha\beta\gamma} x_\beta \sum_i^N \rho_i F_{i\gamma} + \Gamma_\alpha (F_i) + \frac{1}{2} \varepsilon_{\alpha\beta\gamma} (P_{\beta\gamma} - P_{\gamma\beta}) (*)$$

Balance for IAM

$$(*) : \underline{x} \rightarrow \underline{x} + \underline{a}, \underline{a} = 0$$

$$\rho \frac{d}{dt} \sigma_\alpha + \partial_\delta \sum_{\alpha\delta} =$$

$$= \Gamma_\alpha (F_i) + \frac{1}{2} \varepsilon_{\alpha\beta\gamma} (P_{\beta\gamma} - P_{\gamma\beta})$$

$$\underline{\sigma} = \text{const}: P_{\beta\gamma} = P_{\gamma\beta}$$

Balance for external AM:

$$\rho \frac{d}{dt} \varepsilon_{\alpha\beta\gamma} x_\beta v_\gamma + \partial_\delta \varepsilon_{\alpha\beta\gamma} x_\beta P_{\gamma\delta} =$$

$$= \varepsilon_{\alpha\beta\gamma} x_\beta \sum_i^N \rho_i F_{i\gamma}$$

## Balance Equation of Energy

$$e = \frac{1}{2} v^2 + u \quad \text{Total energy per unit of mass}$$

$$u \quad \text{Internal energy per unit of mass}$$

$$\phi_{ea} = e \rho v_\alpha + P_{\alpha\beta} v_\beta + J_{u\alpha} \quad \text{Energy Flux}$$

$$J_{u\alpha} \quad \text{Heat flux}$$

$$\sigma_e = \sum_i^N \rho_i F_{i\alpha} v_{i\alpha} \quad \text{Energy supply by mechanical work of external forces}$$

### Material balance(s)

$$\rho \frac{d}{dt} e + \partial_\alpha (P_{\alpha\beta} v_\beta + J_{u\alpha}) = \sum_i^N \rho_i v_{i\alpha} F_{i\alpha}$$

$$\rho \frac{d}{dt} u + \partial_\beta J_{u\alpha} + P_{\alpha\beta} \partial_\beta v_\alpha = \sum_i^N \rho_i v_{i\alpha} F_{i\alpha}$$

### Local balance(s)

$$\partial_t e + \partial_\alpha (P_{\alpha\beta} v_\beta + J_{u\alpha} + e \rho v_\alpha) = \\ = \sum_i^N \rho_i F_{i\alpha} v_\alpha + \sum_i^N F_{i\alpha} J_{i\alpha}$$

$$\partial_t (\rho u) + \partial_\alpha (J_{u\alpha} + \rho u v_\alpha) + P_{\alpha\beta} \partial_\beta v_\alpha = \\ = \sum_i^N F_{i\alpha} J_{i\alpha}$$

## Entropy Balance

$\Delta m$ : Simple thermodynamic system

Exchange of mass, work, heat

Principle of local equilibrium

## Gibbs Fundamental Equation

$$ds = \frac{1}{T} du + \frac{p}{T} d\left(\frac{1}{\rho}\right) - \sum_i^N \frac{\mu_i}{T} dw_i$$

$$+ \frac{1}{\rho T} (E_\alpha d\mathbb{D}_\alpha + H_\alpha d\mathbb{B}_\alpha)$$

$$w_i = \rho_i / \rho, \quad i = 1 \dots N$$

$$du = \dots, \quad d\left(\frac{1}{\rho}\right) = \dots, \quad dw_i = \dots$$

## Material balance

$$\rho \frac{d}{dt} s + \partial_\alpha (\phi_s - \rho s v_\alpha) = \sigma_s$$

## Entropy flow:

$$\phi_{sa} = \frac{1}{T} \left( J_{u\alpha} - \sum_i^N \mu_i J_{i\alpha} \right) + \rho s v_\alpha$$

## Entropy production:

$$\sigma_s = J_{u\alpha} \partial_\alpha \left( \frac{1}{T} \right) + \frac{1}{T} (p \delta_{\alpha\beta} - P_{\alpha\beta}) \partial_\beta v_\alpha +$$

$$+ \sum_i^N J_{i\alpha} \left[ \frac{F_{i\alpha}}{T} - \partial_\alpha \left( \frac{\mu_i}{T} \right) \right] +$$

$$+ \sum_i^N \Gamma_i \left( -\frac{\mu_i}{T} \right) \geq 0$$

## Process Equations (Flux-Force-Relations)

(Eckart-Onsager-Meixner-Prigogine)

Entropy Production (\*):

$$\sigma = \sum_i X_i Y_i \geq 0$$

$TX_i = X_i$  ... Forces

$TY_i = -Y_i$  ... Fluxes

$$Y_i = \sum_k L_{ik} X_k$$


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$$L_{ik} = L_{ki}$$

Onsager (Casimir)-Symmetry

$\|L_{ik}\| \geq 0$  ... 2<sup>nd</sup> Law

Linear Independency of Fluxes ( $Y_i$ ):

$$\sigma = J_{u\alpha} \partial_\alpha \frac{1}{T} + \frac{1}{T} (\rho \delta_{\alpha\beta} - P_{\alpha\beta}) \partial_\beta v_\alpha +$$

Heat Transfer      Internal Friction

$$+ \sum_i^{N-1} J_{i\alpha} \left[ \frac{1}{T} (F_{i\alpha} - F_{N\alpha}) - \partial_\alpha \frac{\mu_i - \mu_N}{T} \right]$$

Diffusion

$$+ \sum_{k=1}^r \Gamma_k \left( -\frac{A_k}{T} \right), \quad A_k = \sum_l \gamma_{kl} \mu_l$$

Chemical Reactions

## Example: Diffusion and Heat Transfer in 2 Component Fluid System (No internal friction or chemical reactions)

Thermostatic EOS

$$T = T(u, \rho_1, \rho_2)$$

$$p = p(u, \rho_1, \rho_2)$$

$$\mu_i = \mu_i(u, \rho_1, \rho_2), \quad i = 1, 2$$

Balance Equations

$$\frac{d\rho}{dt} + \rho \partial_\alpha v_\alpha = 0$$

$$\rho \frac{dw_i}{dt} + \partial_\alpha J_{ia} = 0, \quad i = 1, 2$$

$$\rho \frac{du}{dt} + \partial_\alpha P = \sum_i^2 \rho_i F_{ia}$$

Process Equations

$$J_{ia} = \sum_{k=1}^2 L_{ik} \left( \frac{F_{ka}}{T} - \partial_\alpha \frac{\mu_k}{T} \right) + L_{iu} \partial_\alpha \frac{1}{T}$$

$$i = 1, 2$$

$$J_{ua} = \sum_{k=1}^2 L_{uk} \left( \frac{F_{ka}}{T} - \partial_\alpha \frac{\mu_k}{T} \right) + L_u \partial_\alpha \frac{1}{T}$$

UQ:  $u, \rho_1, \rho_2, \rho, v_\alpha, J_{ia}, J_{ua}$

$T, \mu_1, \mu_2, p$

Boundary- and Intial-Conditions.